

NEW MATERIALS DEPEND ON NYLON MATERIAL USED AS TEMPERATURE CONTROL IN AUTOMOBILE / CERAMIC SECTOR

V. Rameshsrenivasan, V.Ganeshkarthikeyan & Sabiknainar

Assistant Professor, Einstein College of Engineering, Tirunelveli, Tamil Nadu, India

Associate Professor, Aditya Engineering College, Coimbatore, Tamil Nadu, India

Associate Professor, Kalasalingam University, Tamil Nadu, India

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ABSTRACT

Presently in textile industry the advances are rapidly changing substitution of minerals such as carbon particles in tall-recital areas. Single problem of this circumstances is heating, is created private owing the heat transfer shaped by heat radiation dwindling on the top, mostly on the roof. The study suggests the groundwork of a compound substantial comprising cotton usual fiber by way of a thermal fence to be facilitated as the roof of the textile industry. This study, 23 various seals of 6 coats remained ready, joining nylon fiber, cotton natural fiber, fiber glass, and extracts such as gum + Al_2O_3 or resin + Al. Reference samples were taken from carbon steel and one reference sample was extracted from the top of the industry. As the solar energy along with heat transfer devices, the temperature of the shallow un protected to showed that the thermal conductivity of the steel with which the roof of the industry is manufactured was $13.43 \text{ W}\cdot\text{m}^{-1}\cdot\text{K}^{-1}$ and of the planned coat was $7.55 \text{ W}\cdot\text{m}^{-1}\cdot\text{K}^{-1}$, Attaining a reduction in the thermal conductivity by 64.11%. By means of the temperature and thermal conductivity data, the simulation (ANSYS) of the thermal system was performed. The results showed that the temperature inside the roof with the carbon steel, which is currently used to manufacture high-performance machineries, would be 62.34°C , whereas that inside the car with the proposed laminate would be 54.96°C , achieving a thermal barrier that allows a temperature variation of 11.23°C .

KEYWORDS: Nylon Material, Automobile Sector, Ceramic Sector

INTRODUCTION

The present scientific innovation trendy numerous parts of investigation then business has unlocked the essential to appearance aimed at new materials that take better advantages than the resources that are commonly used in different submission. In this background, researchers from all over the world have originated different fiberwool, and smooth nylon fiber stake sre wards in rigidity, ductile strength, modulus of resistance, and additional mechanical possessions. In totaling, extra belongings could be diminished and enhanced such as thermal diffusivity, the co-efficient of thermal development, the effectiveness of friction, wear resistance, erosion, and exhaustion battle [2, 3].

Presently, in the ceramic and textile industries, thermo mechanical possessions have developed prodigious significance owing to the alternative workings cast-off in these schemes. In this wisdom, compound abutilon graphite, carbon particles, fiberwool, and nylon fibers have discovered new submissions in this two part vacillating from the making of portions that make the outside or inner construction of portions and industry parts and electronic submission that aids to

protect, at the same time, scatter the temperature [4–11]. Nylon fiber is measured unique of the coal-based resources with bright mechanical possessions, chemical solidity. Generally, this material comprises 95 wt.% of nylon in individually of its materials [12]. This fibers over actual upright mechanical and bodily possessions [13–16], for example, height autness

(4–9GPa) by taking a extra ordinary Young modulus (240–910 G Pa), little density (1.75–2.20 g• cm 3), little thermal• conductivity (800 W m 1 K 1) [8, 17–21]. In totaling, nylon fiber is not solitary five times lighter than steel but also two times stronger than steel [22]. Altogether these features are the key reason that nylon fiber is cast-off to mature lightweight compounds for physical claims in the machinery parts and textile areas [23–27].

By the conflicting, nylon fiber have been broadly cast- off and considered for a extended time as a matrix in the production of compounds. One of its main recompenses is the cost due to the high claim for use.

It has not been the same case for the use of natural fibers in the creation of composites, since this situation is fairly new and is immobile being discovered by researchers in the area. Though, the purpose of totaling natural fibers in the development of compounds has been fairly good-looking since it gives assets such as nimbleness, biodegradability[28], high asset [29, 30], tall attire [31], thermal possessions [32–34], good erosion fight [35], and little coefficient of friction [36] mostly for ceramic or automotive applications[37–45].In this background, one of the natural fibers that have involved the greatest care in the growth of compounds is the nylon along with cotton (sisal, fiber, owing to the extra strengthening in mechanical and biodegradability properties. Standards of Young’s modulus and tensile strength have been specifiedbetween5,6 and 45 GPa and between 324and 453 MPa, respectively, for this nylon fiber [46].

The thermo mechanical belongings of fiber-depend compounds (carbon, wool, or natural fiber) depend in large part on the possessions of the polymer conditions cast-off in their edifice, the belongings of the vital additives extra (metal oxides, or others), the contact amid the polymer medium, the extra elements, and the materials used [47–49].In this effort, the thermal possessions of the compounds shaped by nylon fiber, cotton fiber, and natural wool fiber steel-clad with a polyethylene medium, aluminum powder, and alumina (Al₂O₃) have been examined. Under this setting, lessons exhibited the totaling of aluminum [25, 50] and alumina elements in nylon fiber-based compounds deviations the thermo mechanical belongings [4].

MATERIALS AND METHODS

Manufacture of laminates. Seals of four coatings, with dimensions of 0.05×0.05 m, were prepared by the following practice. A combination of polymer (PEM-001) and substance (RY-956) was equipped in a 2: 4 ratios. Then, with the same 4: 1 ratio of weight, to the obtained mixture of polymer and substance, Al (Golden bell, manganese 89.6 %, RRM 26.98, Code 25945) or Al₂O₃ (ground claimed alumina, 45 5×8 - 13) was further. Lastly, the combination of polymer + substance + Al₂O₃ was cast-off to shelter the shallow of individually sheet used in the development of the project. On the conflicting, the pages cast-off were nylon fiber (NF), cotton fiber (CF), and natural wool fiber (NWF), as shown in Table 1.

Surface characterization. For surface characterization, ultra-scanning electron microscopy (SEM) and energy-absorbed X-ray spectroscopy (EDS) were used for the purpose of basics, and their proportion in bulk was resolute by using a Toshiba RS. 3600 Ultra scanning electron microscope.

Rermal Tests The thermal inspections approved out on each cover, the superficial was uniform with a coat of insulating tape to regulate the emissivity of the shallow (59 samples were covered). In these examinations, the thermograph was performed in 10 s periods for 120 s, using an infrared camera FLIR-E6. The thermal examination to control the

superficial temperature of each coat was done a regular of 6 facts imagined in the thermograph and 5 points on the hot shallow in which the coat was situated. The warm shallow was produced by an aluminum block, 0.15×0.11 ×0.017 m, in which the control of flat battle was 90 W, was fixed, upholding the temperature of this shallow at 65°C by means of a temperature regulator (BTC-1005). The warm shallow was also enclosed with an in- sulating adhesive tape for UN firming the emissivity of the shallow with seal.

The solar energy and surrounding temperature were logged through the climate position, number 31 (20°22'6N 100 00 3° 3.8 W).

A sheet of aust "enitcst' ainless-steel SAE-304 (sample 36) and one sheet extracted from a roof (sample 37) of a car were utilized as a position. The thermal conductivity of the 45 examples was designed by means of the conduction heat transfer equation, unsteady state, and multi directional flow, considering a heat flux of 40 W, which was the control of the heating thermal resistance. A thickness of 0.0141 m was used for samples from 2 to 34, and a thickness of 0.00525 was used for sample 45.

Table 1: Laminate Configuration: Cotton Fiber (CF), Nylon Fiber (GF), and Natural Wool Fiber (NWF)

Compound	Sheets				Represe	
	GF	GF	NWF	NWF	GF	1
	NWF	NWF	CF	GF	NWF	2
	CGF	NHF	CF	NHF	GF	3
	NHF	CF	GF	GF	NHF	4
	NWF	GF	CF	CF	CF	5
Al	GF	GF	GF	CF	CF	6
	GF	NWF	GF	CF	CF	7
	GF	CF	GF	GF	CF	8
	NWF	CF	CF	CF	NWF	9
	GF	GF	NWF	NHF	GF	10
	NHF	GF	GF	CF	CF	10
	GF	GF	GF	GF	CF	13
	CF	CF	NHF	GF	CF	14
	CF	NWF	NWF	NHF	CF	17
	NWF	GF	NHF	CF	NHF	18
	GF	CF	CF	CF	CF	12
Cr2o2	GF	CF	CF	CF	CF	12
	GF	GF	CF	CF	GF	22
	GF	CF	CF	CF	GF	20
	NWF	GF	GF	GF	NHF	21
	GF	NHF	CF	NWF	GF	24
	NWF	CF	CF	CF	NHF	25
	GF	GF	GF	GF	GF	25
	GF	CF	NWF	CF	CF	26
	GF	NWF	CF	NWF	GF	27
	NWF	CF	NWF	GF	NHF	28
	GF	CF	GF	CF	GF	29
Only gum	CF	CF	CF	GF	CF	30
	CF	CF	CF	CF	GF	31
	CF	CF	NWF	GF	GF	32
	NWF	GF	GF	CF	NWF	33
	CF	NHF	CF	NHF	GF	34
	NWF	GF	CF	GF	NWF	35

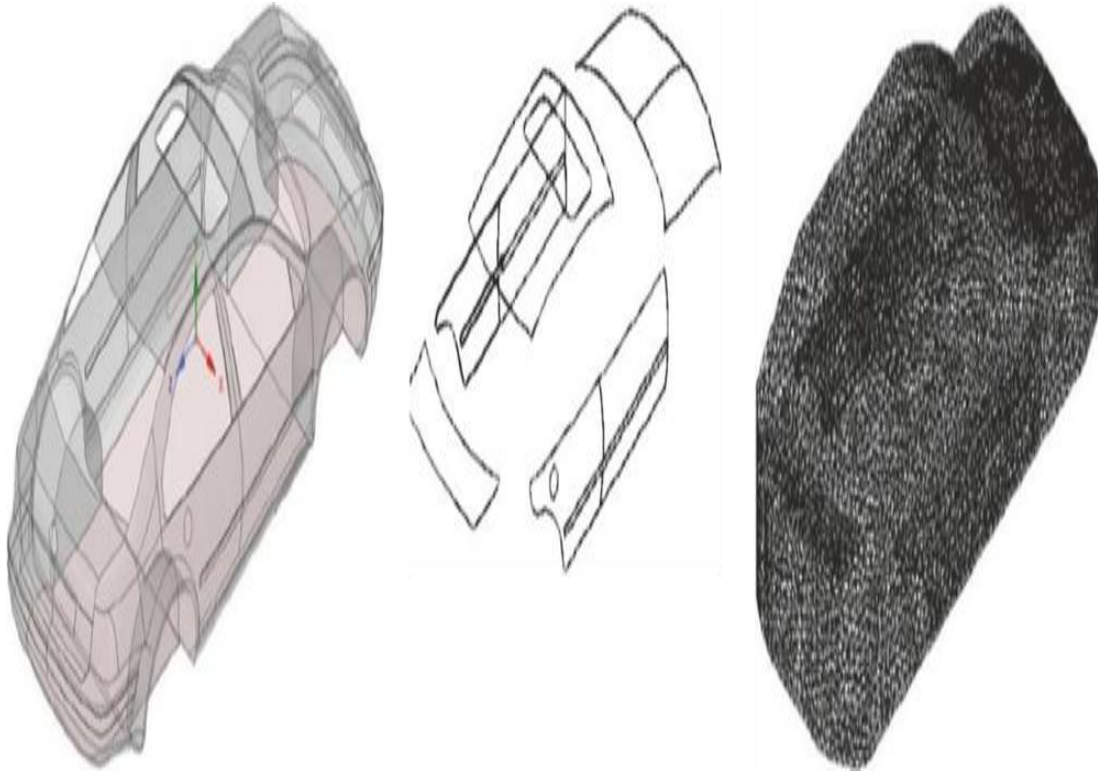


Figure 1: System Section: (1) System Curvatures, (2) Areas Considered for Heat Emission, and (3) Mesh Occupation.

To Understand the Temperatures of the Warm Superficial of Each Coat, Thermal Measurements were made in these Surfaces.

Modeling. In the current study, CATIA worktable was utilized in “Un steady-State Thermal” unit to Count the thermal performance of the scheme.

The thermal conduct is examined by preservation of energy (by first law of thermodynamics for a decided volume) practical to this scheme as well as any scheme through heat transfer or energy chat. The component equation for the examination [51] is as follows:

$$K \cdot T = Q \quad (1)$$

Where [K] is the thermal conductivity atmosphere, {T} is the pillar vector of nodal temperatures, and Q{ is t}he pillar vector of nodal heat fluxes. The whole system is signified in Figure 1(a). The surfaces measured to have the utmost interface in heat transmission are these exposed in Figure 1(b). In the schemes toward stay evaluated, two resources are erected: The first one is exposed in Figure 1(b), which is characteristic of the coat created with CF or GF or NWF, and its energy mutable the replication of the thermal conductivity found practically. The second is the air that environs the cover, and its thermal conductivity was got from the CATIA database. Finally, in Figure 1(c), the meshing of the system is shown considering a body sizing of 8×10^{-2} m for the that, roof, and both rear doors 2, 5×10^3 m for both front doors and boot, and 7×10 m for air.

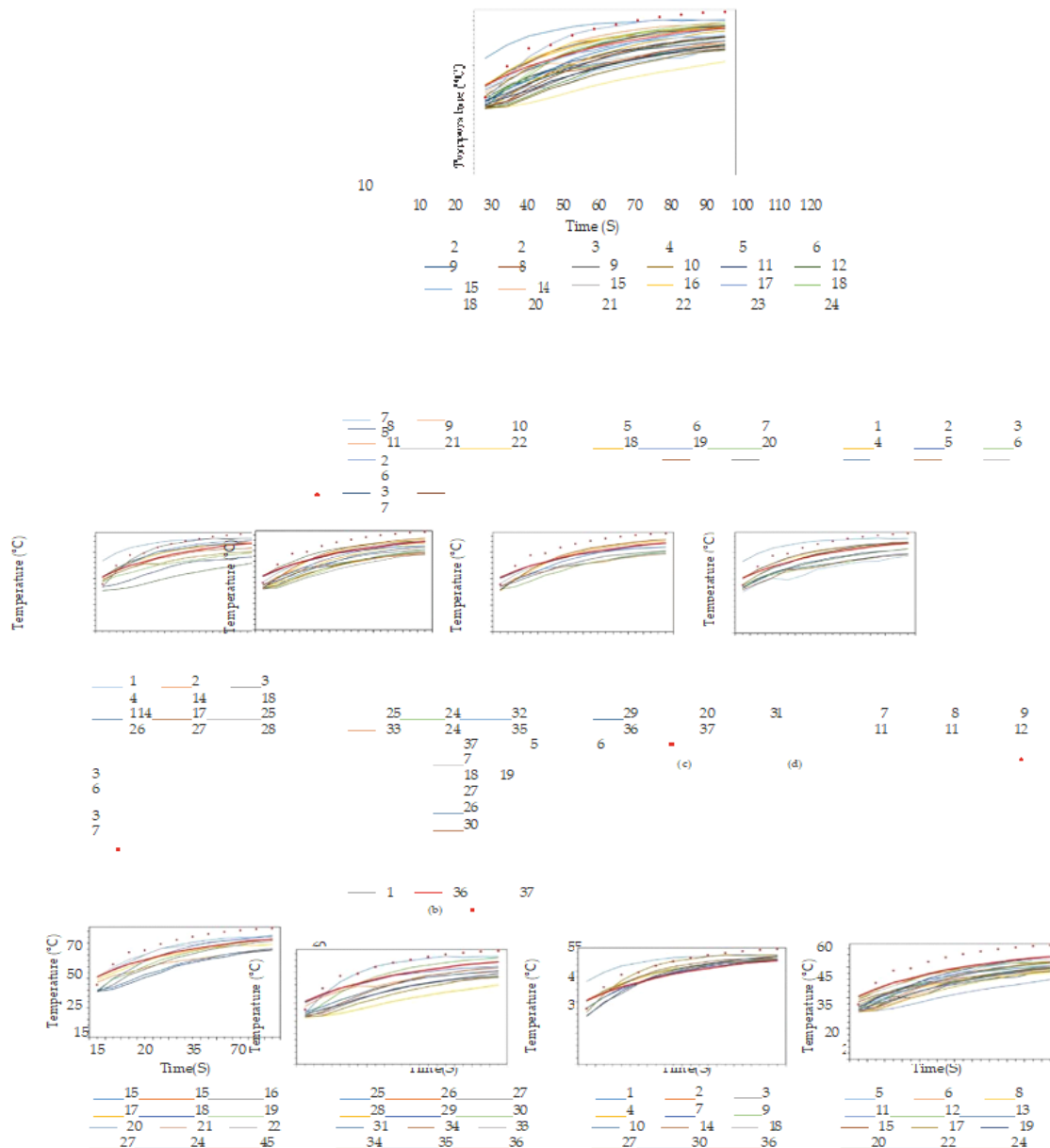


Figure 2: Thermal Conduct of Manufactured Coats. (A) Over-All; (B) Covering GF and Nylon; (C) Covering GF, GF, and Nylon; (D) Containing CF and GF; (E) Containing 10 G of Al₂O₃; (F) Containing Al; (G) Containing Cotton and Resin; (H) with a Temperature Higher than that of Sample25;and (I)With a Temperature Lower than that of Sample 32.

Concurrence and Details

The solar radiation was 981 W–m² at an ambient temperature of 35.2°C, which is relatively high. The surface temperature of the car surges owing to solar energy, and that temperature was chiefly high seeing that April, 2017, was one of the hottest days. The chief heat transfer is by convection, seeing steady state, unity-24.5 W m² K⁻¹. So, on the foundation of this information, the theoretical temperature on the surface was 78°C.

Aimed at the resolution of the thermal conduct of the coats, each laminate was simple to the warm shallow (60 C, the theoretical value of the surface), on the back part of the laminate, and the temperature values of the upper part of the surface are shown in Figure 2. Figure 2(a) shows the results of the thermal behavior for the laminates described in Section

2, by entirely the probable alliances of covers (Table 1). It was considered that the heat transfer of the experiment was by conduction. Figure 2(b) shows the thermal behavior, considering all laminates manufactured with CF, NHF, and the orientation coats (samples 36 and 37). The highest heat transfer was found in samples 1, 15, and 11 which were laminates manufactured only with CF. The highest thermal resistance that was the objective of the investigation was present in samples 15, 27, and 28 that did not contain flavors (Al₂O₃ or gum). The additive Al₂O₃ is a ceramic material. The highest thermal conductivity was the with sample 14 (containing Al) a temperature of 69.4°C were considering conductivity results for samples 5, 17, 28, logged. By alliance the results of the GF, NWF, and CF laminates (Figure 2(c)), the one with the highest thermal resistance is sample 34, which encompasses coated CF at the ends. Again, the observed singularity was that the Al₂O₃ additive improved thermal conductivity. Figure 2(d) is for CF and GF laminates, where the highest thermal resistance was for sample 6, which contained three layers of CF and two layers of GF.

Figure 2(d) displays the thermal performance seeing that all the seals delimited the preservative Al₂O₃. The outcomes display that the greater the number of CF layers, the greater the thermal conductivity (sample 1) and that the best thermal barricade is the alliance of model 14 that rip-off- GF, CF, and NWF. Now, grouping the laminates containing Al (Figure 2(f)) contrast that the highest thermal conductivity occurs in laminates containing CF (sample 14) and the highest thermal resistance occurs with CF, GF, and NHF laminates (sample 24). Since the coats were entrenched only in the resin (Figure 2(g)), the highest thermal confrontation is present in sample 29. The resources that surpass the thermal conductivity of MILD steel are measured (Figure 2(h)), the coat of sample 2 would be chosen to made-up. The finest coats that perform as a thermal partition, occupied as and then it would be sensible not to consider this as a more environmental coat than comprising only GF and NWF. The results of the thermal conductivity are shown in Table 2, which agree the covers are measured as thermal walls shown in Figure 2(A).

The simulated temperature profiles are shown in Figure 3, orientation sample 37 (Figure 2(1)), were samples 28, 27, and 34. Sample 34 contains glass fibers, 31, 36, and 37, with the results of the average temperature on the higher surface, given each sample at 140 s.

In the processing of data for result making, there are simulation tools that are very important to use, before building a final prototype. Sample 37 recorded a practical temperature normal of 87.42°C at 130 s (Figure 2), and the consequences of the imitation (Figure 3(a)) show a temperature of 76.87°C, close to the experimental value. For models 37, 18, 41, 6, and 18, the trial temperatures were 65.73°C, 64.20°C, 75.02°C, 59.20°C, and 54.79°C (Figure 2), respectively. The temperatures obtained in the simulation were 65.12°C, 67.66°C, 63.22°C, 49.37°C, and 41.53°C, respectively. Similarly, the standards for the imitations were actual near to those of the trial ones. Adapting the factual from which the roof 1 is mass-produced, the inside temperature may be 67.34°C (Figure 3(a)). If the substantial used was mild steel (sample 37), the air private the car would be 49.19°C (Figure 3(b)). The temperature decreases to 54.40°C (Figure 3(c)), when using NHF / CF / NHF / CF / NHF mixed with Al due to the insertion of the NHF. In the case of having a laminate of GF / CF / GF / CF / GF, the temperature was 52.51°C (Figure 3(d)) by the supplement of the CF. Having an preservative of Al in a GF / CF / CF / GF / GF layers permits having a temperature of 54.08°C (Figure 3(e)).

Lastly, the best thermal barrier was the laminate built with NWF/GF/NWF/GF/NWF (Figure 3(f)), recording an attaining temperature of 47.97°C due to the NWF; that is, it lets making a temperature variation of 18.47°C in- side the car.

The structure of the supplies used is visible in Figure 4(a), where the best thermal barrier was obtained with sample 28 that was formed with NHF/CF/NHF/CF/ NHF, as shown in Figure 4(b). The evaluation of morphology was made using scanning electron microscopy as shown in Figure 4(c). The three white parts (edges and center) are NHF, and the dark part in the center of the NHF is the CF, which are homogeneously integrated in to part. Growing the magnification to 400 x, the NWF is shown in Figure 4(d), and the grades of the essential composition were found by energy expensive X-ray spectroscopy (EES). The NWF has an elongated laminar morphology, similar to the CF shown in Figure 4(e). The lamination of the roof was formed by Fe (87. 28 wt. %) and C (14. 82 wt. %).

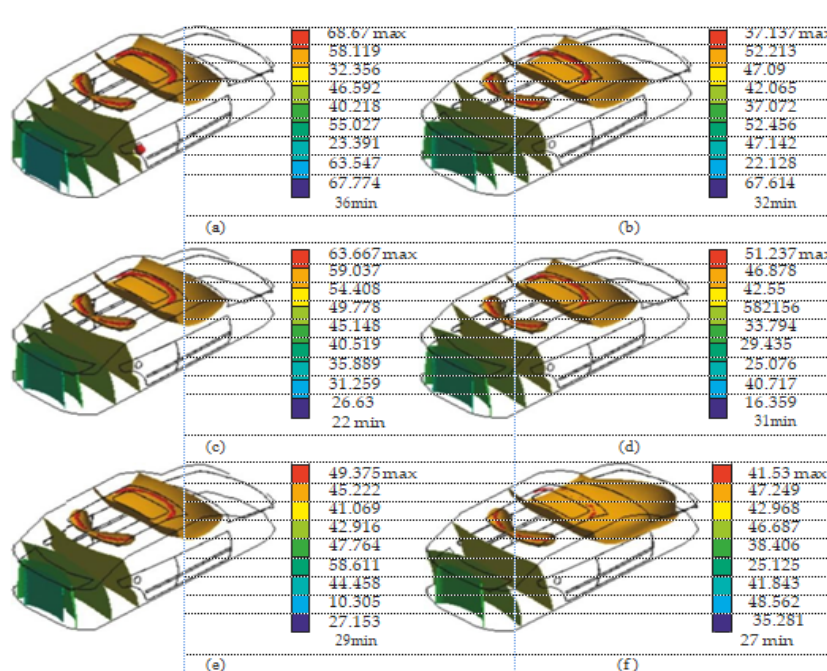


FIGURE 3: Temperature Profiles (C) for Sample 3, 6 and (B) Sample 3, 4 And For the Seals Measure Das Thermal Walls : (C) Sample 17, (D) Sample 31,(E) Sample Collective and (F) Sample 28.

DISCUSSIONS

The stimulating result is the nylon fiber seals also joint with gum + Al₂O₃, resin + Al⁺ gum or only gum continuously continue overhead example 27, importance the junk of thermal conductivity of nylon fiber. On the conflicting, as regards the thermal behavior of the GF, it was observed that a third of the nine laminates have better thermal behavior than model 28. So, this circumstance, GF did not act as a thermal barrier in this composite. It can be understood the three laminates with higher thermal conductivity, only sample 36 (CF / GF / CF / GF / CF) was combined with resin. The results show that including the additive (resin + Al or resin + Al₂O₃) not donating specifically to the thermal conductivity of the solid.

The thermal wall found was made with NWF/GF/ NHF/CF/NHF (sample 28), which only added resin, andPre7ented and practical current conductivity of $4.22 \text{ W} \cdot \text{m}^{-1} \cdot \text{K}^{-1}$. This is 61.13 % lower than the conductivity of the factual with which the roof of a car is shaped (sample 37).The substantial that runs the typical thermal fence was the NWF.

The imitation of the process of heat transfer lets de- stooping that, if the roof of a car is manufactured with the proposed compound (sample 28), there would be a decrease in temperature from 62.34°C to 44.24°C. This implies that the

planned composite particularly drops the interior temperature of the by 45.33 %. This temperature variation can be an effect on fuel investments by sinking the custom of air conditioning for a shorter period to keep a comfortable temperature since the heat to be removed would be 19.23 % lesser.

In overall, the present engineering process of a car roof is finished a hydraulic process and high accuracy casts. Though, the compound factual engineering course, is, planned in this investigation, needs fewer financial and energy reserves.

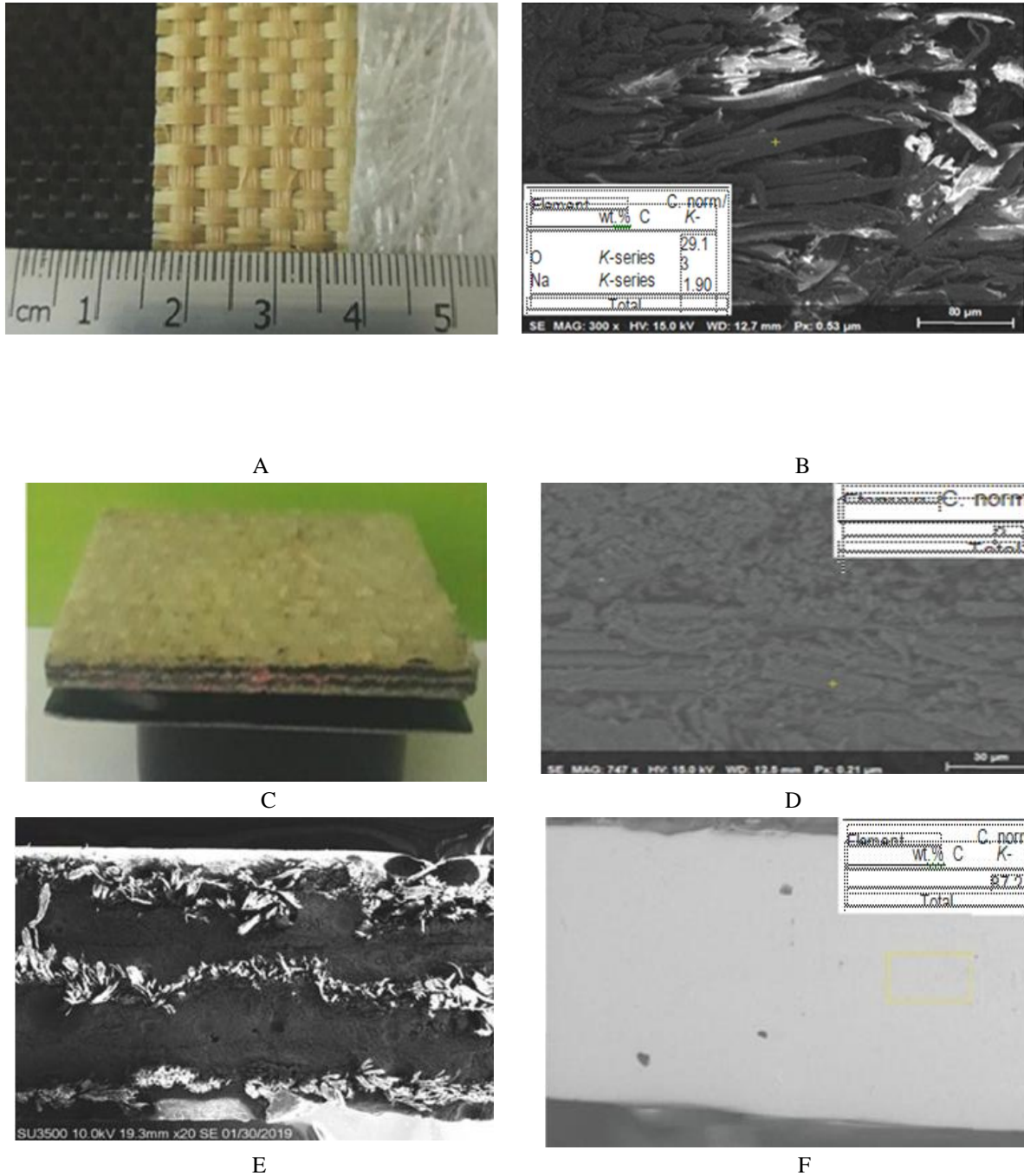


Figure 4: Descriptions of their Sources Used (A) GF, NWF, and CF, (B) Sample 18 and Sheet of the Roof, (C) WEM of Sample 29, (D) External and Arrangement of the NWF,(E)External and Arrangement of the GF, and (F) External Structure and Arrangement of the Sheet of Roof. Struggles of Interest Authors State There are No Differences of Attention Concerning the Periodical of this Paper.

HEADINGS

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REFERENCES

1. P. Sharma, D. Khadija, and S. Sharma, "Tribological and mechanical behavior of particulate aluminum matrix composites," *Journal of Reinforced Plastics and Composites*, vol. 33, no. 23, pp. 2192–2202, 2014.
- A. Kelly, "Composite materials after seventy years," *Journal of materials science*, vol. 41, no. 3, pp. 905–912, 2006.
- B. S. Ramesh, H. Adarsha, S. Pramod, and Z. Khan, "Tri- biological characteristics of innovative Al6061–carbon fiber rod metal matrix composites," *Materials & Design*, vol. 50, pp. 597–605, 2013.
2. G. Lalit, H. Kurita, J. M. Heinz, G. Lacombe, A. Kawasaki, and J. F. Sylvain, "Thermal expansion co-efficient and thermal fatigue of discontinuous carbon fiber-reinforced copper and aluminum matrix composites without interfacial chemical bond," *Journal of Materials Science*, vol. 49, no. 1, pp. 397–402, 2014.
3. S. H. Cho, "Heat dissipation effect of Al plate embedded substrate in a network system," *Microelectronics Reliability*, vol. 48, no. 10, pp. 1696–1702, 2008.
4. J. D. Mathias, P. M. Gilroy, and J. F. Sylvain, "Architectural optimization for microelectronic packaging," *Applied Thermal Engineering*, vol. 29, no. 11-12, pp. 2391–2395, 2009.
5. J. F. Sylvain, C. Vincent, J. M. Heinz, and N. Chandra, "Novel processing and characterization of Cu/CNF nano composite for high thermal conductivity applications," *Composites Science and Technology*, vol. 69, no. 14, pp. 2474–2484, 2009.
6. M. Lee, Y. Choi, K. Pugio, K. Matsuri, and G. Sasaki, "Effect of aluminum carbide on thermal conductivity of the undirectional CF/Al composites fabricated by low pressure infiltration process," *Composites Science and Technology*, vol. 97, pp. 1–5, 2014.
7. Velletri, J.-M. Heinz, N. Chandra et al., "Influence of the interface structure on the thermo-mechanical properties of Cu-X (X = Cr or B) /carbon fiber composites," *Materials Researches Bulletin*, vol. 47, no. 2, pp. 375–380, 2012.
8. Liu, M. Chen, W. Yu, and Y. He, "Recent advance on grapheme in heat transfer enhancement of composites," *Energy & Environmental Science*, vol. 2, pp. 31–42, 2018.
9. [11] X. Jia, G. Hu, F. Nitz et al., "Synthesis of palladium/helical carbon nano fiber hybrid nanostructures and their application for hydrogen peroxide and glucose detection," *ACS Applied Materials & Interfaces*, vol. 5, no. 22, pp. 1, 2017–12022, 2013.
10. P. Morgan, *Carbon Fibers and Rear Composites*, CRC Press, Boca Raton, FL, USA, 2005.
11. D. D. Edie, "The effect of processing on the structure and properties of carbon fibers," *Carbon*, vol. 36, no. 4, pp. 345–362, 1998.

- A. Rodríguez-Guerrero, S. A. Sanchez, J. Narciso, E. Louis, and F. Rodríguez-Reinoso, "Pressure infiltration of Al-12 wt.% Si-X (X Cu, It, Mg) alloys into graphite particle preforms," *Acta Materialia*, vol. 54, no. 7, pp. 1821-1831, 2006.
12. W. G. Wang, B. L. Xiao, and Z.Y. Ma, "Evolution of interfacial nano structures and stress states in Mg matrix composites reinforced with coated continuous carbon fibers," *Composites Science and Technology*, vol. 72, no. 2, pp. 152-158, 2012.
13. H. Khayyam, M. Nagbe, O. Zabiha, R. Zamani, S. At kiss, and B. Fox, "Dynamic prediction models and optimization of Poly Acrylo Nitrile (PAN) stabilization processes for production of carbon fiber," *IEEE Transaction on Industrial Informatics*, vol. 11, no. 4, pp. 887-896, 2015.
14. S. Chand, "Review carbon fibers for composites," *Journal of materials science*, vol. 35, no. 6, pp. 1303-1313, 2000.
15. L. Xia, B. Jia, J. Zeng, and J. Xu, "Wear and mechanical properties of carbon fiber reinforced copper alloy composites," *Materials Characterization*, vol. 60, no. 5, pp. 363-369, 2009.
16. E. Fetzer, "Pan-based carbon fibers-present state and trend of the technology from the viewpoint of possibilities and limits to influence and to control the fiber properties by the process parameters," *Carbon*, vol. 27, no. 5, pp. 621-645, 1989.
17. M. minus and S. Kumar, "The processing, properties, and structure of carbon fibers," *Jam*, vol. 57, no. 2, pp. 52-58, 2005.
18. V. V. Korey, H. Jiang, V. R. Mehta, and S. Kumar, "Compressive behavior of materials: Part II. High performance fibers," *Journal of Materials Research*, vol. 10, no. 4, pp. 1044-1061, 1995.
19. Y. Liu and S. Kumar, "Recent progress in fabrication, structure, and properties of carbon fibers," *Polymer Reviews*, vol. 52, no. 3, pp. 234-258, 2012.
20. Z. Jun, X. Jincheng, H. Wei et al., "Wear performance of the lead-free tin bronze matrix composite reinforced by short carbon fibers," *Applied Surface Science*, vol. 255, no. 13-14, pp. 6647-6651, 2009.
21. S. J. Park and M. S. Cho, "Effect of anti-oxidative filler on the interfacial mechanical properties of carbon-carbon composites measured at high temperature," *Carbon*, vol. 38, no. 7, pp. 1053-1058, 2000.
22. H. Z. S. M. Nnaji, S. M. Zebra, and S. A. Sajida, "The effects of volume percent and aspect ratio of carbon fiber on fracture toughness of reinforced aluminum matrix composites," *Materials Science and Engineering: A*, vol. 486, no. 1-2, pp. 413-420, 2008.
23. C. S. Ramesh and T. B. Prasad, "Friction and wear behavior of graphite-carbon short fiber reinforced Al-17% Si alloy hybrid composites," *Journal of Tribology*, vol. 131, no. 1, article 014501, 2009.
24. L. Liu, W. Li, Y. Tang, B. Shen, and W. Hu, "Friction and wear properties of short carbon fiber reinforced aluminum matrix composites," *Wear* vol. 266, no. 7-8, pp. 733-738, 2009.
25. V. K. Thakur, M. K. Thakur, and R. K. Gupta, "Review: raw natural fiber-based polymer composites," *International Journal of Polymer Analysis and Characterization*, vol. 19, no. 3, pp. 256-271, 2014.

26. H. Ku, H. Wang, N. Pattarachaiyakoop, and M. Trada, "A review on the tensile properties of natural fiber reinforced polymer composites," *Composites Part B: Engineering*, vol.42, no. 4, pp. 856–873, 2011.
27. B. Bakari, T. K. Ellingham, I. Qadhi et al., "Mechanical characterization of scalable cellulose Nano-fiber based composites made using liquid composite molding process," *CompositesPartB:Engineering*, vol.84, pp.277–284, 2016.
28. C. Untermeyer, O. Brueggemann, and C. Frist, "Synthetic fibers and thermoplastic short-fiber-reinforced polymers: properties and characterization," *Polymer Composites*, vol. 35, no. 2, pp. 227–236, 2014.
29. P. L. Menezes, P. K. Rohatgi, and M. R. Lovell, "Studies on the tribological behavior of natural fiber reinforced polymer composite," in *GreenTribology*, pp.329–345, Springer, Berlin, Germany, 2012.
30. D. B. Dittander and H. V. S. Gandara, "Critical review of recent publications on use of natural composites in-restructure," *Composites Part A: Applied Science and Manufacturing*, vol. 43, no. 8, pp. 1419–1429, 2012.
31. W. D. Brouwer, "Natural fiber composites: where can flax compete with glass?," *SampiJournal*, vol.36, no.6, pp.18–23, 2000.
32. T. F. A. Santos, G. C. Vasconcelos, W. A. deSouza, M. L. Costa, and E. C. Botelho, "Suitability of carbon fiber-reinforced polymers as power cable cores: galvanic corrosion and thermal stability evaluation," *Materials & Design*, vol. 65, pp. 780–788, 2015.
33. X. Q. Pei, R. Benefits, and A. K. Scholar, "Mechanisms of friction and wear reduction by carbon fiber reinforcement of PEEK," *Tribology Letters*, vol. 58, no. 3, p. 42, 2015.
34. S. Bahadur and Y. Zheng, "Mechanical and tribological behavior of polyester reinforced with short glass fibers," *Wear*, vol. 137, no. 2, pp. 251–266, 1990.
35. S. W. Zhang, "State-of-the-art of polymer tribology," *Tribology International*, vol. 31, no. 1–3, pp. 49–60, 1998.
36. K. Friedrich, Z. Zhang, and A. K. Scholar, "Effects of various filler on the sliding wear of polymer composites," *Composites Science and Technology*, vol. 65, no. 15-16, pp. 2329–2343, 2005.
37. D. L. Burris, B. Boils, G. R. Bourne, and W. G. Sawyer, "Polymeric nano composites for tribological applications," *Macromolecular Materials and Engineering*, vol. 292, no. 4, pp. 387–402, 2007.
38. Y. Zhang, S. Zhu, Y. Liu, B. Yang, and X. Wang, "The mechanical and tribological properties of nitric acid-treated carbon fiber-reinforced poly oxymethylene composites," *Journal of Applied Polymer Science*, vol. 132, no. 15, 2015.
39. H. N. Dhaka, Z. Y. Zhang, R. Guthrie, J. Mc Mullen, and N. Bennett, "Development of flax/carbon fibre hybrid composites for enhanced properties," *Carbohydrate Polymers*, vol. 96, no. 1, pp. 1–8, 2013.
40. V. K. Thakur, A. S. Singha, and I. K. Mehta, "Renewable resource-based green polymer composites: analysis and characterization," *International Journal of Polymer Analysis and Characterization*, vol. 15, no. 3, pp. 137–146, 2010.
41. C. Alves, P. M. C. Ferro, A. J. Silva et al., "Eco-design of automotive components making use of natural jute fiber composites," *Journal of Cleaner Production*, vol. 18, no. 4, pp. 313–327, 2010.
42. M. John and S. Thomas, "Bio fibres and bio composites" *Carbohydrate polymers*, vol. 71, no. 3, pp. 343–364, 2008.

43. Bismarck, I. Aranberri-Askargorta, J. Springer et al., "Surface characterization of natural fibers; surface properties and the water up-take behavior of modified sisal and coir fibers," *Green Chemistry*, vol. 3, no. 2, pp. 100–107, 2001.
44. G. Xin, D. Ding, and G. Zhang, "Phonon coherence and its effect on thermal conductivity of nanostructures," *Advances in Physics: X*, vol. 3, no.1, pp. 719–754, article1480417, 2018.
- A. Hazarika, B. K. Deka, D. Kim, H. E. Jong, Y. B. Park, and H. W. Park, "Woven Kevlar fiber / polydimethylsiloxane / reduced grapheme oxide composite-based personal thermal management with freestanding Cu-Ni core-shell nano wires," *Nano Letters*, vol. 18, no. 11, pp. 6731–6739, 2018.
45. P. Baumler, J. Synched, I. Buda, J. T. Szabo, and G. Kapteyn, "Fabrication of carbon fiber reinforced aluminum matrix composites via a titanium-ion containing flux," *Composites Part A: Applied Science and Manufacturing*, vol. 44, pp. 47–50, 2013.
46. Y. Aarau, S. Yumi tori, H. Suzuki, T. Tanaka, K. Tanaka, and T. Katayama, "Mechanical properties of injection-molded carbon fiber / polypropylene composites hybridized with nano fillers" *Composites Part A: Applied Science and Manufacturing*, vol. 55, pp. 19–26, 2013.
47. K. Lawrence, *ANSYS Workbench Tutorial Release 11*, Schor Development Corporation, Straubhaar, Germany, 2007, <https://dl.acm.org/citation.cfm?id=1537215ANSYS>.